

## Three-level DC-DC Converter with GSS based MPPT for PV Applications

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**Abstract:** The DC-DC converters are widely used in photovoltaic generating systems as an interface between PV module and the load. These converters must be chosen to be able to match the maximum power point (MPP) of PV module when climatic conditions change with different resistive load values. So DC-DC converters must be used with MPPT controller in order to reduce losses in the global PV system. The nonlinear power characteristic of PV greatly depends on the environmental conditions. Hence in order to draw maximum available power, various algorithms are used with PV voltage/current or both as an input for the maximum power point tracking (MPPT) controller. Non-isolated DC-DC converters with high voltage gain are desired in all photovoltaic (PV) energy conversion systems. The three-level boost converter provides the high voltage transfer which enables the high power PV system to work with low size inductors with high efficiency. The balancing of the voltage across the two capacitors of the converter and MPPT is achieved using a simple duty cycle based voltage controller. Detailed simulation of three-level DC-DC converter topology with GSS algorithm is carried out in MATLAB/SIMULINK platform. The validation of the proposed system is done by the experiments carried out on hardware prototype of 100 W converter with low cost ATmega328 controller as a core controller. The proposed system will suit as one of the solutions for PV based generation system and will show high performance, such as a conversion efficiency of up to 94%.

**Keywords:** Golden section search, Incremental Conductance, Maximum power point tracking (MPPT), Perturb & Observe, Three-level boost converter

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### I. Introduction

The world's energy consumption is increasing by about 3.5% annually and is expected to rise further because of population growth and demanding modern lifestyles. The increased energy demand results in rapid depletion of conventional fossil fuels and adds to the existing consequences of the environmental pollution. Solar energy—for all practical purposes as a source of energy, is inexhaustible, absolutely free (in terms of its availability), quiet, and environmentally friendly. In order to reduce the overall cost of PV systems, therefore, these are utilized effectively with interface to the existing systems through DC-DC converters. The major challenge is to extract the power under varying operating conditions which influence the output voltage extraction of the maximum power from a solar cell turns out to be a vital consideration for optimal system design.

Under fluctuation of climatic conditions, MPP changes and MPPT must adjust the converter duty cycle to track the new MPP. Therefore, the DC-DC converter must be chosen to be able to match the MPP under different atmospheric conditions. When the duty cycle changes as a result of changed climatic conditions, the boundary of the converter design parameters will change.

Isolated converter structures with cascaded configuration enables to achieve high voltage gain. Three level boost converters have significant advantage as compared to conventional boost converter. The size of the inductor is reduced and switch voltage rating is half of the output voltage. This reduces the overall size and improves the efficiency in three-level DC-DC converters.

The fundamental problem addressed by MPPT is to produce maximum output power under a given temperature and irradiance. Various algorithms for MPPT are reported in the literature and used for the efficient energy conversion process. These methods are derivative based and noise sensitive. Golden section search (GSS) based algorithm is having noise and signal fluctuation immunity with fast convergence as compared to many reported MPPT method is proved in this paper. The proposed system is easy to implement on low cost hardware with single current sensor. The PV connected system with three-level converter using GSS based MPPT is presented in Figure 1.

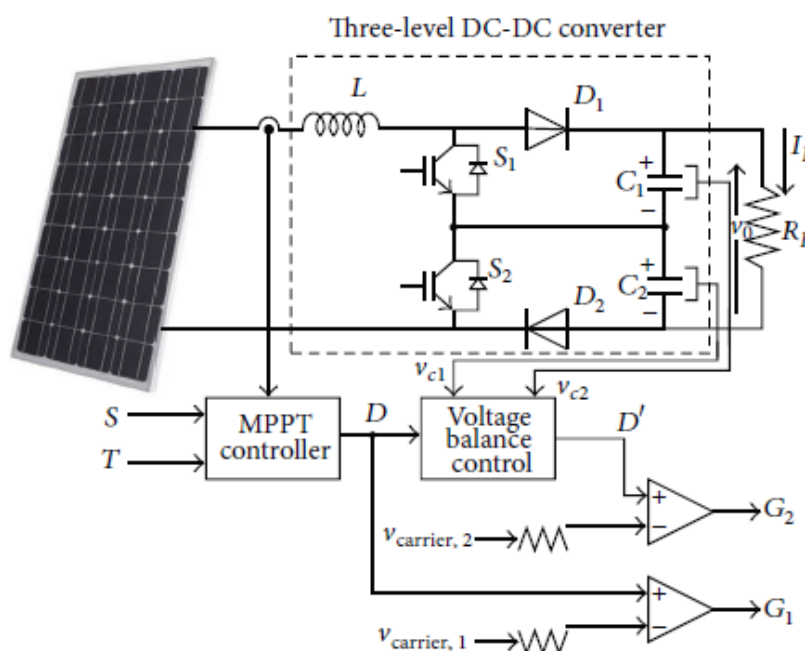


Figure.1 Proposed scheme with PV-fed three-level boost converter

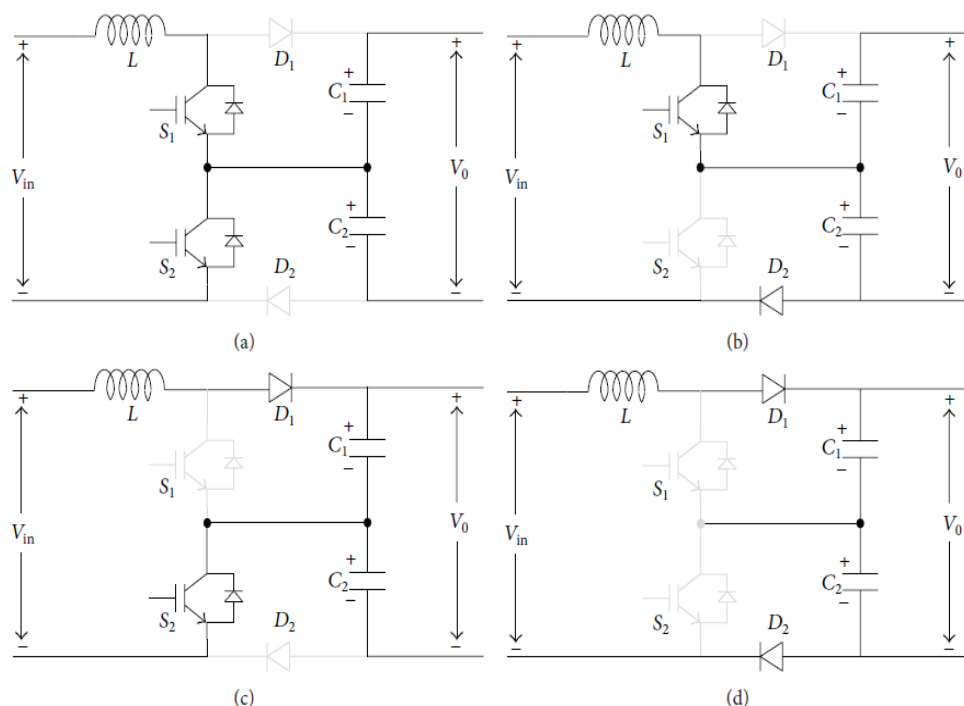
A GSSMPPT based three-level DC-DC boost converter for PV energy conversion system is presented in this paper with a simple duty cycle based pulse width modulation (PWM) and capacitor voltage controller. In the three-level boost converter the switching and reverse recovery losses are less. A hardware prototype of 20W converter is built and the control is made cost effective using ATmega based low cost controller. Both the simulation and hardware results are seen to have clear agreement with inherent robustness built using GSS MPPT algorithm when compared to the existing P&O and Incond.

## II. Three-Level Nonisolated Dc-Dc Converter

To maintain DC bus voltage constant, in high power rating PV systems with high voltage gain requires boost converter with controller. Interfacing PV with boost converter having three-level with wider range of voltage level is preferred due to reduce input filter size and current ripple cancellation. Three-level boost converter have increased power density, efficiency, and reduction in cost as the switching device's voltage rating is half of the output voltage. As the capacitors  $C_1$  and  $C_2$  are equal, voltage of the center point is  $V_o/2$ . This also reduces the voltage stress across the switching devices in these converters.

### 2.1 Operating Principle

In three-level boost converter  $V_{c1}$ ,  $V_{c2}$  are the voltage across the capacitors  $C_1$ ,  $C_2$ , respectively. The switch  $S_1$  is upper switch and  $S_2$  is lower switch and switching frequency is  $f_s$ . In this converter, carrier signals  $V_{carrier,1}$  and  $V_{carrier,2}$  for PWM generation are triangular for both switches but those are in  $180^\circ$  phase shift to each other. With these carrier signals both switches can be turned ON and OFF at the same time. Therefore, the converter operates in four distinct modes as shown in Figure 2.



**Figure.2** Operating modes of three-level DC-DC converter

(1) Mode 1: both switches are turn ON as shown in Figure 2(a) and the voltage across inductor is  $(V_L) = \text{input voltage } (V_{in} > 0)$ . In this mode the inductor is always in charging mode and charged capacitors supply the current to the load.

(2) Mode 2: in this mode  $S_1$  is ON and  $S_2$  is OFF as shown in Figure 2(b) and voltage across the inductor is  $V_L = V_{in} - V_{C_2}$ . In this mode inductor may be in charging mode or discharging mode and charged capacitor  $C_1$  supplies the current to the load while  $C_2$  is in charging mode.

(3) Mode 3: in this mode,  $S_1$  is OFF and switch  $S_2$  is ON as shown in Figure 2(c) and voltage across the inductor is  $V_L = V_{in} - V_{C_1}$ . In this mode inductor may be in charging mode or discharging mode and charged capacitor  $C_2$  supplies the current to the load while  $C_1$  is in charging mode.

(4) Mode 4: both switches are turned OFF as shown in Figure 2(d) and inductor voltage is  $V_L = V_{in} - V_{C_2} < 0$ . Due to boosting operation  $V_{C_1} + V_{C_2} > V_{in}$ , so in this mode inductor always is in discharging mode and both capacitors are in charging mode and input supplies the current to the load.

In modes 1 and 4 inductor is in charging mode and discharging mode, respectively, but in modes 2 and 3 inductor currents raising polarity depend on the voltages  $V_{C_1}$  and  $V_{C_2}$ , depending upon the relation between  $V_{in}$  and half of the output voltage ( $V_0/2$ ); there exist two operating regions.

(1) Region 1:  $V_{in} > V_0/2$

(2) Region 2:  $V_{in} < V_0/2$

In region 1,  $V_{in} > V_0/2$ ; hence  $V_L = V_{in} - V_0/2 > 0$  so inductor current raising polarity is positive in modes 3 and 2 as shown in Figure 3(a). This will occur only when duty ratios of upper switch ( $D_1$ ) and of lower switch ( $D_2$ ) are less than 0.5; in this region both switches must not be ON at the same time. In region 2,  $D_1 = D_2 > 0.5$ ; input voltage is  $V_{in} < V_0/2$ ; then, inductor current raising polarity is negative  $V_L = V_{in} - V_0/2 < 0$  in modes 2 and 3 as shown in Figure 3(b). In this region both switches must not be OFF at the same time.

### III. MPPT Techniques

PV array has non-linear I-V characteristic and output power depends on environmental conditions such as solar irradiation and temperature. The point on the I-V, P-V characteristic curve of PV array where the PV system produces its maximum output power is called as Maximum Power Point (MPP). The purpose of MPPT is to adjust the solar operating voltage close to MPP under changing environmental conditions. In order to continuously gather the maximum power from the PV array, they have to operate at their MPPT despite of the inhomogeneous change in environmental conditions.

There are different types of MPPTs. The conventional MPPTs are generally based on the "hill climbing" method and give an accurate MPP but the time taken to obtain the MPP is larger, thereby resulting in a lesser efficiency. They are also economically favorable.

Modern MPPT techniques are faster and find the MPP with lesser time and by executing a smaller number of cycles as they have the ability to deal with non-linearity and models which are not mathematically defined.

### 3.1 Perturb & Observe Method

In this method, the controller adjusts the voltage by a small amount from the array and measures power; if the power increases, further adjustments in that direction are tried until power no longer increases. This is called the perturb and observe method and is most common, but this method can result in oscillations of power output. It is referred to as a hill climbing method, because it depends on the rise of the curve of power against voltage below the maximum power point, and the fall above that point. Perturb and observe is the most commonly used MPPT method due to its ease of implementation. Perturb and observe method may result in top-level efficiency, provided that a proper predictive and adaptive hill climbing strategy is adopted.

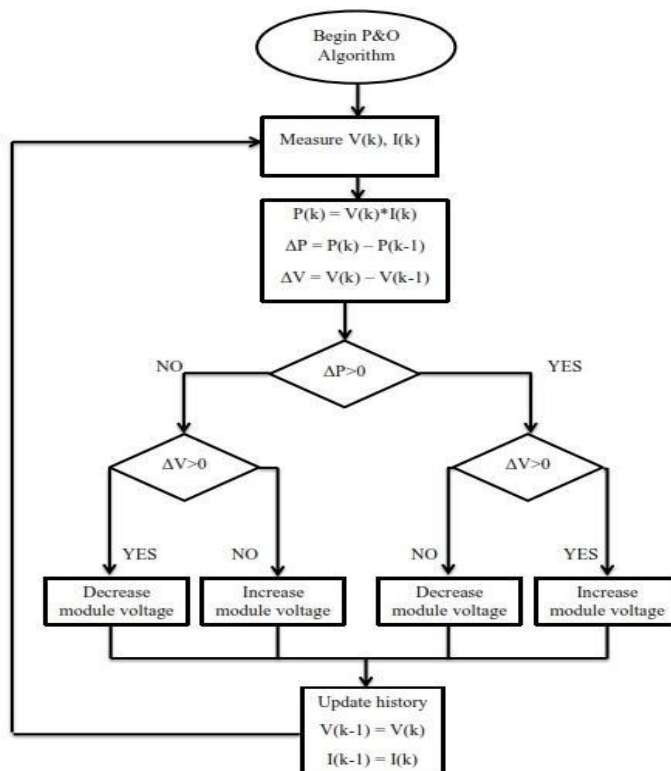


Figure.3 Flowchart of P&O Algorithm

In the P&O algorithm, the inputs of the MPPT system are the power output in watts and the working voltage of the PV module. A perturbation is given to the system and the change in power is observed. If the value of change in power is positive, a similar perturbation is applied in order to check for a higher power. If the change in the power output is negative, then the sign of the perturbation is reversed.

### 3.2 Incremental Conductance

In the incremental conductance method, the controller measures incremental changes in PV array current and voltage to predict the effect of a voltage change. This method requires more computation in the controller, but can track changing conditions more rapidly than the perturb and observe method (P&O). Like the P&O algorithm, it can produce oscillations in power output. This method utilizes the incremental conductance ( $dI/dV$ ) of the photovoltaic array to compute the sign of the change in power with respect to voltage ( $dP/dV$ ). The incremental conductance method computes the maximum power point by comparison of the incremental conductance ( $I_{\Delta} / V_{\Delta}$ ) to the array conductance ( $I / V$ ). When these two are the same ( $I / V = I_{\Delta} / V_{\Delta}$ ), the output voltage is the MPP voltage. The controller maintains this voltage until the irradiation changes and the process is repeated.

The incremental conductance method is derived from the P&O method. In P&O method the ratio of change in power by change in voltage ( $dP/dV$ ) is monitored to track the MPP.

Since,

$$\frac{dP}{dV} = \frac{d(IV)}{dV} = I + V \frac{dI}{dV} \quad ;$$

So, The MPP can thus be tracked by comparing the instantaneous conductance ( $I/V$ ) to the incremental conductance ( $\Delta I/\Delta V$ ).

In In Cond method, the working voltage and current of the PV module is monitored using different sensors. Using these values, the instantaneous conductance ( $I/V$ ) and the incremental conductance ( $\Delta I/\Delta V$ ) are computed and their ratio is compared in order to trace the MPP of the system. In comparison to the P&O method the value of power output is not considered.

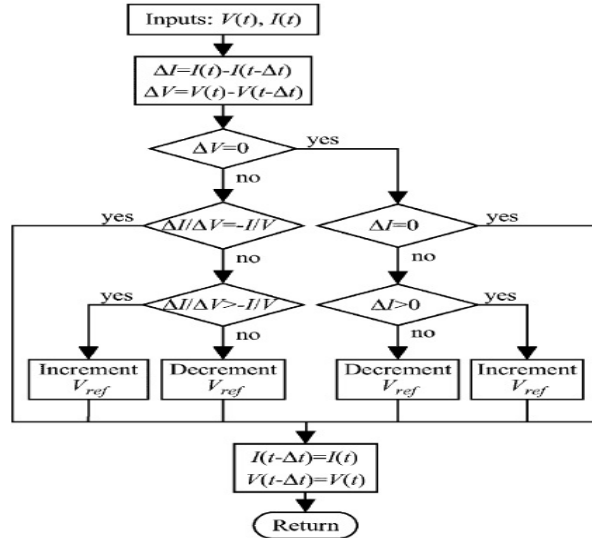


Figure.4 Flowchart of Incremental Conductance

### 3.3 Golden Section Search Algorithm

The golden section search is a technique for finding the extremum (minimum or maximum) by successively narrowing the range of values inside which the extremum exists is known to exist. The technique derives its name from the fact that the algorithm maintains the function values for triples of points whose distances form a golden ratio. The algorithm is the limit of Fibonacci search for a large number of function evaluations. Fibonacci search and Golden section search were discovered by Kiefer in 1953.

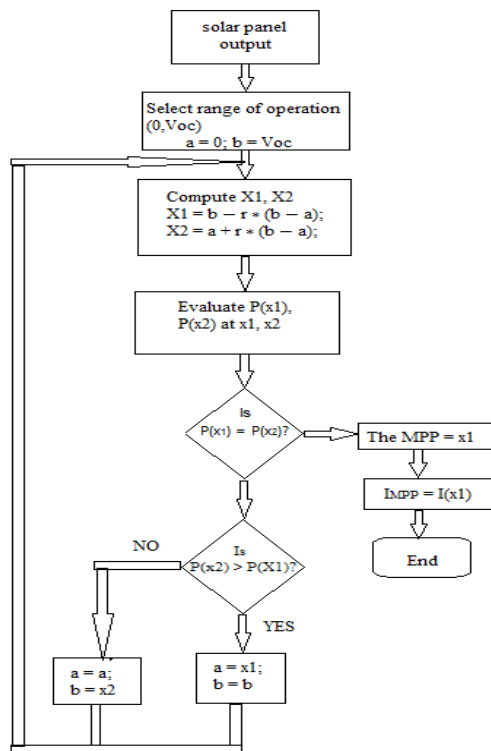


Figure.5 Flowchart of GSS Method

#### IV. Proposed MPPT Scheme

##### 5.1 Golden Section Search Principle

For a GSS based MPPT for photovoltaic system, the  $P$ - $V$  characteristics are the operating characteristics wherein  $f(x)$  corresponds to power, whose maximum value has to be tracked. The range of operation is from zero to open circuit voltage ( $V_{oc}$ ); that is,  $a = 0$  and  $b = V_{oc}$  as shown in Figure.6(b). The way of tracking maximum point is shown in Figure.7. The voltage corresponding to the maximum power is obtained and mapped into the  $V$ - $I$  characteristics to obtain the current reference.

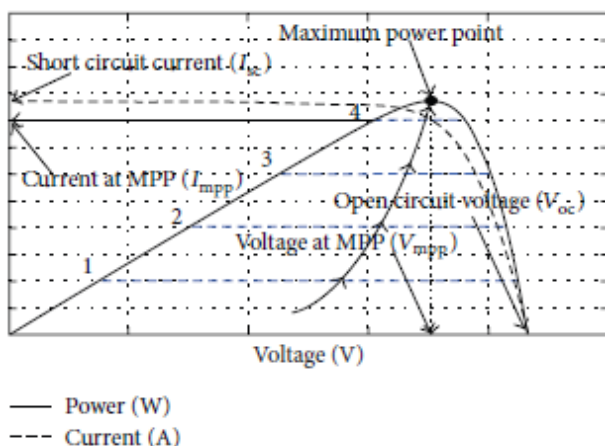


Figure.6 (a) MPPT tracking with GSS algorithm

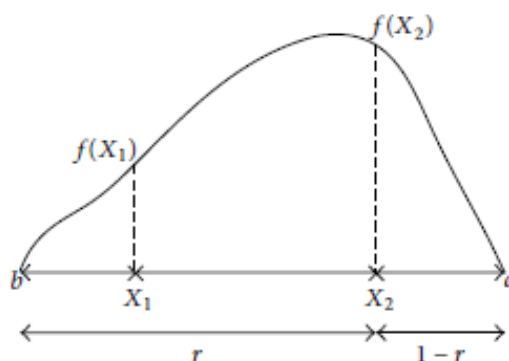


Figure.6 (b) Division of interval on the characteristics

The main aim is to find maximum functional value of  $(x)$  within the input interval  $[ab]$ . Two points  $x_1$  and  $x_2$  are selected in the interval  $[ab]$  and function  $(x)$  is evaluated at these points. Points  $x_1$  and  $x_2$  are selected such that each point subdivides interval into two parts and length of whole line/length of larger fraction = length of larger fraction/length of smaller fraction. Assume a line segment  $[0, 1]$  as shown in Figure 6(b).

Then,

$$1/r = r/1-r;$$

that is,

$$r^2 + r - 1 = 0; \text{ hence } r = 0.618.$$

Consider  $x_1 = b - (b-a)$ ; that is,  $x_1$  is 0.618 of interval away from  $b$ .

Consider  $x_2 = a + (b-a)$ ; that is,  $x_2$  is 0.618 of interval away from  $a$ .

For a GSS based MPPT for photovoltaic system, the  $P$ - $V$  characteristics are the operating characteristics wherein  $(x)$  corresponds to power, whose maximum value has to be tracked. The range of operation is from zero to open circuit voltage ( $V_{oc}$ ); that is,  $a = 0$  and  $b = V_{oc}$  as shown in Figure 6(b). The way of tracking maximum point is shown in Figure 6. The voltage corresponding to the maximum power is obtained and mapped into the  $V$ - $I$  characteristics to obtain the current reference.

The inductor current feedback is used to generate the error by comparing it with the reference current  $I_{MPP}$  generated by the GSS algorithm and it is processed through proportional (P) controller.

This P controller changes the duty ratio ( $D$ ) according to error and governs the PV to track the maximum power point on its characteristics. Figure 7 shows the block diagram of GSS MPPT based reference generator.

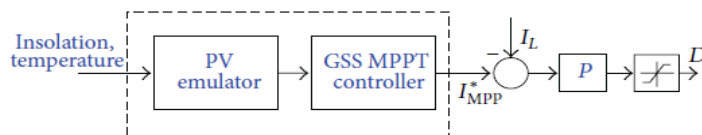


Figure.7 GSS MPPT

##### 5.2 Voltage Balancing Control

Even though both capacitor values  $C_1$  and  $C_2$  are equal, there is a voltage unbalance between output capacitors ( $V_{c1}$  and  $V_{c2}$ ) due to mismatch of two real capacitors and equivalent series resistance. The voltage balancing controller is required to maintain the equal voltages across these capacitors through duty cycle control and is implemented as shown in Figure 8.  $G_1$  and  $G_2$  are the gate pulses for switches  $S_1$  and  $S_2$ , respectively. In the three-level boost operation of the DC-DC converters with duty ratio relates the fact that the input and output voltage are given as

$$V_0/V_{in} = 1 / (1 - 0.5d_1 - 0.5d_2);$$

If  $d_1 = d_2 = D$ , then

$$V_0/V_{in} = 1 / (1 - D);$$

where the input DC voltage  $V_{in}$  is PV input voltage and varies with respect to varying environmental conditions. The duty ratio of the boost switch  $S_1$  is determined by the MPPT control ( $D$ ) and duty ratio of the boost switch  $S_2$  is determined by the additional controller. The PI generates the duty ( $D$ ) from the voltage error obtained from  $(V_{c1} - V_{c2})$ .

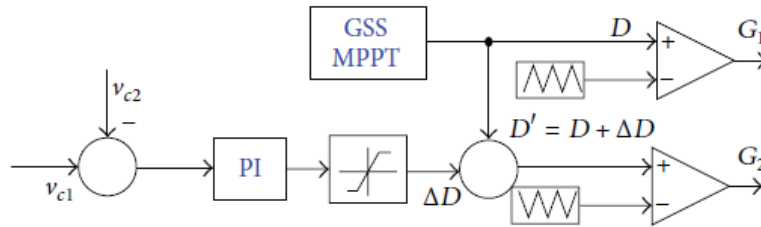


Figure.8 Block diagram of MPPT with voltage balance control

Consider

$$\Delta D = Kp + [Ki(V_{c1} - V_{c2})] / s;$$

where  $Kp + Ki/s$  is the transfer function of the PI controller. The duty cycle  $D' = D + \Delta D$  controls switch  $S_2$  of the converter to balance the voltage across the capacitors.

### V. Simulation Results

The proposed MPPT method is compared with Perturb and Observe and Incremental Conductance based MPPT techniques. It is observed that the iterations required for the GSS are 4-5 nos. as other methods take 7-8 nos. The simulation circuit for incremental conductance and P&O algorithms are same and is shown in the figure.9. The output waveforms obtained for the both the Incond and P&O are almost the same. The area between the panel output and converter output gives the gain of the system. The simulation circuit for GSS is shown in figure.13. The proposed scheme is implemented in ATmega328 controller with GSS based MPPT and duty ratio control.

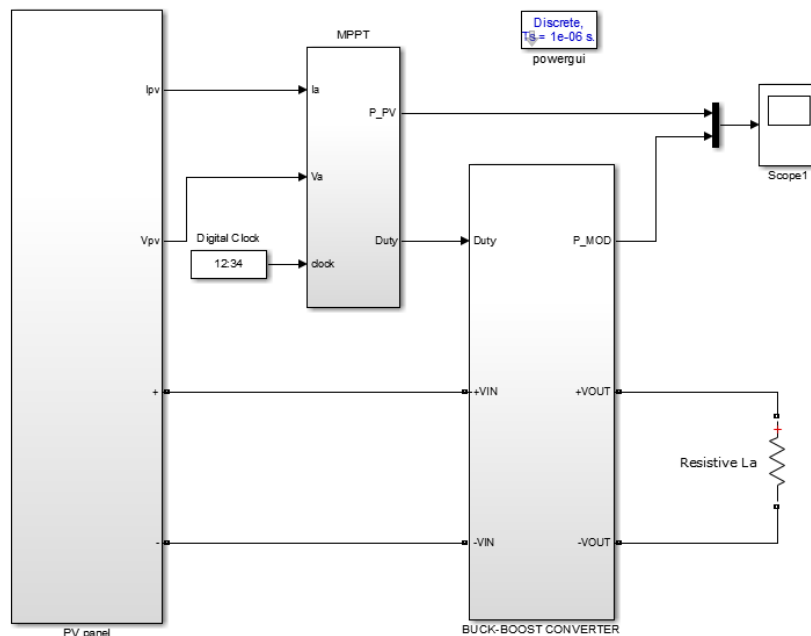


Figure.9. Simulation Circuit for Incond and P&O

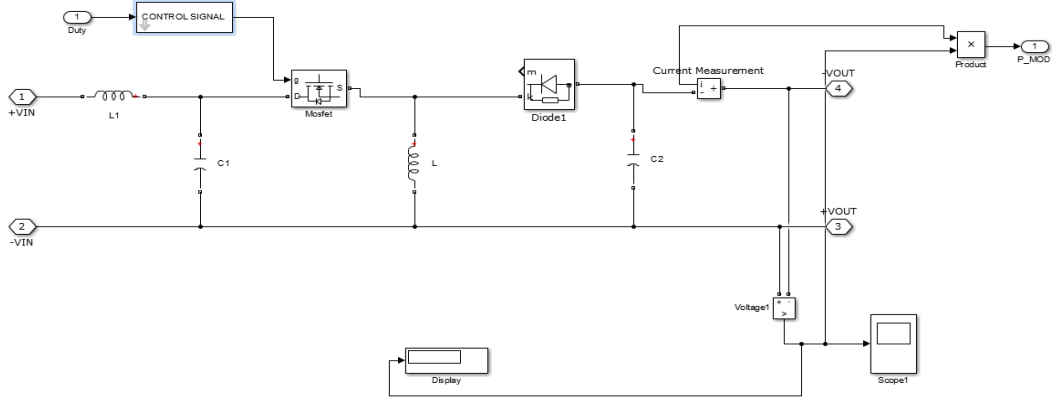


Figure.10. Buck-Boost converter

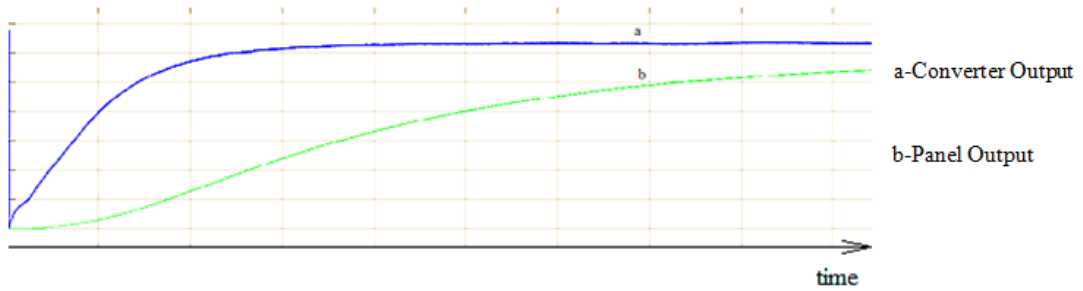


Figure.11. Output Waveform of Incond

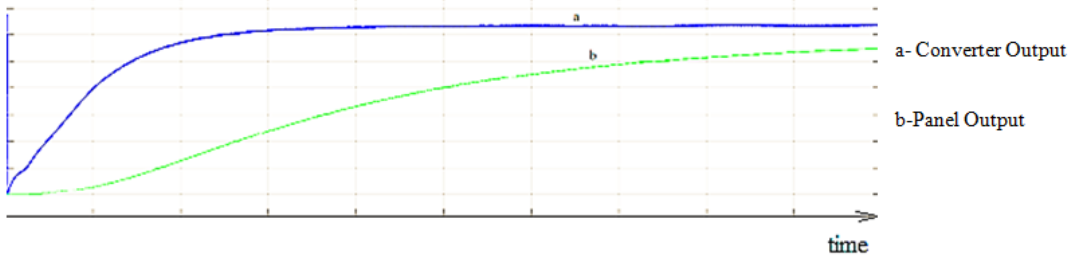


Figure.12. Output Waveform of P&O

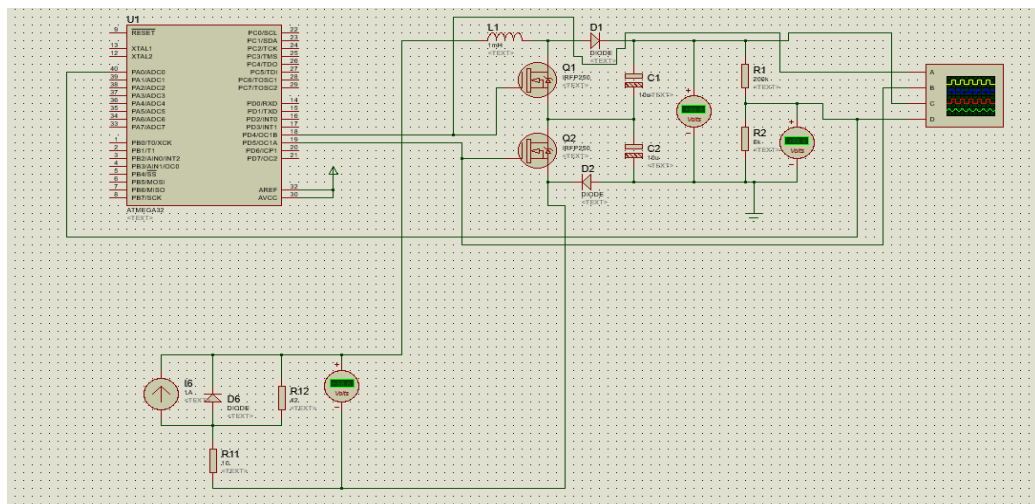


Figure.13. Circuit diagram for implementation of GSS



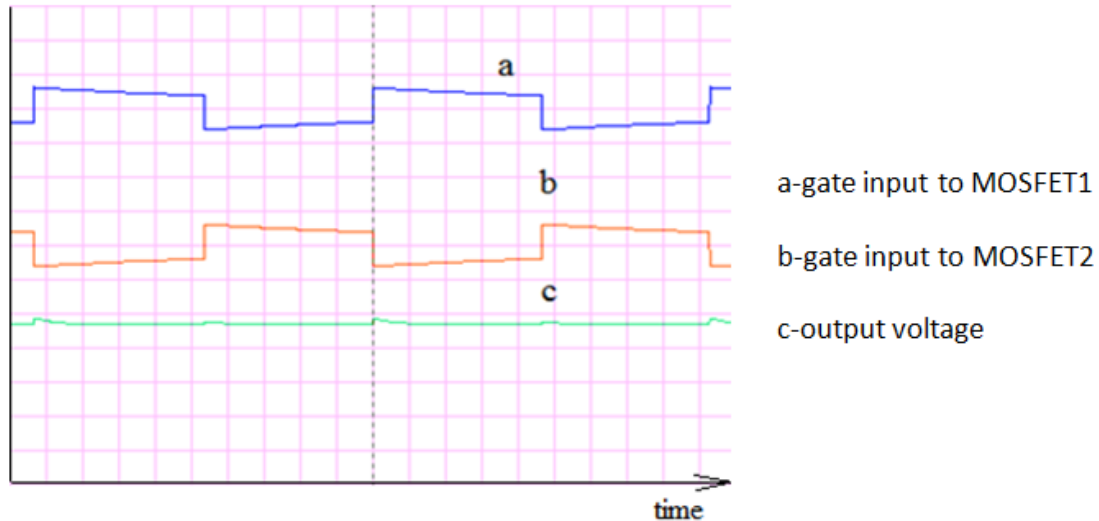


Figure.14.Output waveforms of GSS

## VI. Conclusion

The three-level boost converter is used to interface the PV system for maximization of the power extraction. Various maximum power point tracking algorithms- P&O, InCond and Golden Section Search were compared in the simulation and found that GSS algorithm shows the better dynamic response with the faster convergence without any oscillations while tracking. So the hardware was implemented using GSS algorithm. The voltagebalancing of the DC bus is executed through the PI controller and performance is observed to be satisfactory.

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